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# **99目揃えプリプレグ及びその製造法**

**②特** 

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明 細 当書

1. 箔明の名称

引指をプリブレグ及びその製造法

- 2. 特許別來の範囲
  - (1) 一方向に並行するマルチフィラメントの機能の束の複数個を互いに発達し、かつその磁線及方向にこれら来間及び東内でフィラメントと結らみ、かつ銀雄が超脂で含みしてなる引線をフリブレグ。
  - (2) マルチフィラメントの密線の東の投数値を一方向に並行して互いに関ジさせ、得られる 磁性の取の災合体に高圧液体を吹き付け、吹き付け時又は吹き付けをにその趣経の京の築 合体に傾距を含受させることを特徴とする引 跡えブリブレグの製造法。
- (3) 説体が水、水と空気との混合物、有機密鉄及び合成研節のいずれかである特許頭求の第 図第2項の引摘とアリブレグの複数法。
- (4) 派件の圧力が80~500㎏/のってある特

新聞求の範囲第2項又は第5項配数の引力を ファブレグの整弦法。

- (6) 放体が水、水と空気との混合物、有四溶解及び合成研胞のいずれかである物質語中の総数の影響を対しているのではなる。
- (7) 流体の圧力が50~500kg/cm5である特許弱次の範囲第5項又は終6項配数の引提生プリプレグの超流法。

(1)

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(2)

#### 8. 処明の詳細を説明

本発明は 202 強化プラスチンク の 成形材料として用いられる引搬をフリプレグに関するものである。

磁熱強化プラスチック用のブリプレグは不敬 亦炊、ナーン状、クロス状又はチョップストラ ンド状の既離、或は一方向に引揃えた繊維、又 はこれらを摂み合わせたものに熱硬化性問題を 含泛したもので、得られたブリプレグはこの級 遊に用いられた繰艇によつてそれぞれの特徴が 生じ、その特徴に応じて各種の用途に向けられ ている。

これらのブリプレグのうち、一方向に引摘えた 戦福を用いて得たプリプレグは容易に薄いシート状、ケーブ状のものが得られるため長尺の 破状体、 破層板等の 成形材料として好趣で、 例 2 はゴルフのクラブシャフト、 スキーのボディ 炎のレジャースポーツ用品や自動車、 航空機材などの 孤独 放金 はおに用いられている。

従来、との烈のプリプレクは一方向に引加え

(3)

成形品としての品質が低下するが漢を有している。

本処明の目的は機械的ストレス及び又は無愛 化によって機能と歯器との結合力が低下せず、 マルチフィラメントの繊維の取と束との個に関

(5)

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たマルチフィグメントの類雑の東に倒脂を含せ し、その調磁の軍の複数個を同方向にそれぞれ の車が耳いに改談するように並べてとれら段総 の車と束とをとれら取に含没させた切別によつ て接合してシート状又はテーブ状の形状に成形 するととにより称られている。

(A)

頭が生じにイル・引揃をプリプレク及びその製造 法を提供するにある。

本発明の他の自的は収扱い、巡쓢、成形加工 又は保管によつて品質低下しない引加えブリア レグ及びその設造法を提供するにある。

不死明のさらに他の目的は概能効化プラスチック壓品に用いた場合、その製品の概能引縮を 方向とその直角方向の効度を増大し得、かつそ の他の路特性をパラコかせない引揄えブリンレ グ及びその製造法を遊供するにある。

本発明者は東記目的を選成するため極々研究した結果完成したもので、その引胡をブリブレグの特徴は一方向に並行するマルチフィラメントの職権の取の複数個を互いに関接し、かつその機能の取内及び東面でフィクメントが他のが機能は10月75回に、時間で含役されてなるにのである。

本発明に用いられるマルチフィクメントの東 はフィラメントが多数本級合してなる認識の東 でもつて、英級した長幽維の東からなるヤーン

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(6)

又はトク値が好ましい。

この 級雄には従来の 別揃えブリプレグに用いられる 級雄が用いられ、これを示せば下記の辺りである。

- (1) 有機協能:ナイセン(ポリアミド系)、レ・ ーヨン(セルローズ系)、ピニロン(ポリピ ニルアルコール系)等
- (2) 有機耐熱機能: 芳香飯ポリャー、ポリペンズイミダソール、ポリフルオロカーポン、ポリナミド、フエノール、ポリフエニレオキソシアソール、ピスペンズイミダソペンソフエナンスロウイン、ポリチアジアリール、ポリピチアソール、ポリイミド等の樹脂協能
- (3) 無機嫌疑にガラス、望化ホウ素、アルミナ、空化ケイ素、アスペスト、ジルコニア、シリコンカーバイド、反素(皮素質、風鉛質、耐炎質を含む)等の機能、
- (4) 金属鐵額:クングステン合金、ペリウム、 第合金、鉄、アルミニウム塩の繊維、

(7)

流体に水、又は水と空気との混合物を用いる場合には前体のコストが安く、流体の回移換する必要とせず、また作契環境が日本であるが一方有機溶験や合め歯匿を用いた場合には流体を吹きつけ袋の配換工具が個単であるか又はたれを全く必要とせず、吹き付け工程に受いて連続してマトリンクス用としての問題を含みさせるしたができる。谷に合成砂路を十分に吹き付け

(9)

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- (6) '(1)~(5)で示した戦器のうち二額以上組み合わせたもので、勢に町独住、柴麸性に賞むものが好ましい。

このさいに用いる高圧旅体には、水、水と空気との混合句、有機複雑(何をはメザルアルコ

(8)

た場合には「職権を改めて母間に召放することなく、 吹き付けて得られたものを単にローラー 掛けを行う可贬で繊維の束の内部に母脂を含没 させることができる。

磁線東面に高圧流体を吹きつけるには機能引 節を方向に対して政角に機能東面上超岩太間路 に設けたノスル孔から複数する方法が採られる。

ノズル孔径の大さ及びその機能までの間隔及びノズル酸はフィッメントの大さ及び概念層の厚みなどによつて異なるが、ノズル孔径は1mm以下、物に05~005が好ましいが、これが分り大くたると多量のフィクメントが可吹に続いて持むため、機場の東が乱れ易く、厚さ6不均一となり引動之の効果が失なわれる。

ノズル孔と図典 東面との距離は高圧流体の圧力、機能のノズル孔に対する相対移動速度、機能フィラメントの大き及び東の厚き等によって 定められるが1~15年程度が目安となる。

高圧流体の圧力もまたノズル孔の大さ、ノズ ル孔と螺旋京面との距離、繊維のノズル孔に対

<del>-355-</del>

Ω¢

する相対移動液度フィチメントの定さ及び組織の肌の呼みたどによつて限定されるが50~60km/cm\*であるととが好ましい。圧力が50km/cm\*未満であるとフィチメントの転位が少なくて繊維の束と束との係合が不十分であり、またも00kg/cm\*を超えるとフィチメントの破断が多くケベ立ちが放しくなる。

なびに叫いられる可能にはフェノール付別、 不協和ボリエステル問題、エポキシ母語等の無

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以の取り付ける簡単で協能に対<u>地</u>工器力を掛け 以いのでフィタメントの結み度合を自由に関整 することができる。

つざに本発明の引揃えアリプレグの製造法の ~ 実施放松を閉ばついて説明する。

が1~30においてクリールのフィック・ス・リールのリールのリールのリールのリールのリーをメンフィック・ス・リールのリースのマルチックにさいてクリールのリースのマルチックにでは、カーのでは、

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特別 昭52-151362(4)

硬化性母配びボリイミド耐能、ポリベンズイミグソール供配、ポリフェニレン樹脂、フリーデルクラフト母的母の耐熱性樹脂が用いられ、使用するに当つて粘度を低下させるため加温したり、またこれに有機を供及び又は拾択剤を添加して用いられる。

さらに協能の取断にお圧流体を吹きつけるさい,その底圧流体が吹きつける破離の取断の政 断に近接して、かつこの機能の取断と平行に当 て仮を歌け、この当て板によつてさらに一度高 圧死体をはね返して再び機能の取に衝突させる とフィラメントの複称が能率よく行をわれる。

この当て板には炭面がは性平沿で流体を反射してあるようにされ、金盤、ブラスチンク、ガラス、木、硬質ゴム等で製作される。韓強は全く大部を有しない平板又は円筒、又は遊ら一部6 図に示すように飼食、格子状もしくは短冊状の大部を有するものが用いられる。

当て板を用いると、螺絲の束をとの上に配列して、この当て板を利用するので繊維の束の抑え

02

協権の東に吹き立立た高圧流体をとれた当てて はね返し再び践権のフィラメントに当てそれを 配位させ、高圧流体を効率よく使用する。

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また、第1~第2回において 8 位型ボルで概 継収の移行する方向に対して収角に往復運動させる。

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本务明の引掠をプリプレグは第7 図に示すようにこれが得成されている協議の東 1 \* と東 1 \* との間、及びその東内でフィラメント 2 \* の一 然又は大部が転位して終み合つているので、第 B 図に示す従来届とは異なり機械的ストレス及

02

水のジェット殻の乗件

ノズル直径 D. 2 ma p

正 力 mex 200ky/cm³(40图/分の 既能)

ノズルの先端とヤーンとの距離 B m/m ノズルの個数 1ヶ

ノズル移動迎座 4.5 m/mkm(引触之方 向と直内の方向へ移動し、 5 m/mの巾で企道に没り吹き付けた)

水のジェット流の吹き付け工程後、処理した 炭災級艦の一部を採り、その特性を避定した が吹き付け工程前と比较して引張強度、引張 弾性学には全く低下は見られなかつた。

・ は進の受る方向に対して世央方向の東回破断頭皮は吹き付け工器的ではのであったが吹き付け工器をでは200g/1の中となった。

このようにしてかられたシートを10cで、2時間乾燥後メチルエチルケトンを溶剤としたエポヤン砂節(エピコート#838,100

特別昭52-151362向 び熱ストレスにより、 数維と樹脂との結合力が 低下せず、 とれにともたい磁線の東と東との間 に間瞭が生じないので、取扱い、 選組加工、 又 は保留によつて品質が低でしない。 またこれを 用いて磁線強化プラスチック製品とした場合、 観路氏方向の強度低下がほとんどなく、 定決 に符られた製品に比して製能の引摘え方向及び その直角方向の強度が1.5~4倍も増大させる とができる。

つぎに本発明の突絡製役を実施例で説明する が本発明はこれらによって限定されるものでは ない。

#### 奖施例 1

120007イタメント、4800デニールの炭素繊維(引張競皮350kg/mm<sup>2</sup>、引張 併性率204/m<sup>3</sup>)のフィラメントヤーンを100本を未製の平板の上に0.10g/dの競力を扱けて引強えて並べた、この引力をたってつまる次の条件で水のジェット流を吹き付けた。

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部 B F . MEA 文 P H R 、 MEK 150 P H R ) に 含 设 し、 ついて 1 20 C で 1 5 分 間 乾燥 した。 との 0.1 四 厚 の 引 揃 え ブリ ブレ グッート を 1 方 向 で 被 層 し 1 5 0 × 8 0 × 3 四 の 寸 法 で 成 形 し た。 と の 時 の 致 産 仕 給 鍵 方 向 引 殺 敢 座 ( σ ⊁ ) は 1 9 3 以 / 四 ° 、 協 能 と 近 角 方 向 引 毀 敢 座 ( σ ェ ) は 8.4 以 / 四 ° で あ つ た。 と の 時 の 極 総 体 複 舎 将 準 は 6 1 % で あ つ た。

#### 实施例 2

水のジェット流の圧力をも00kg/cm とした以外は実施例1と同じ条件で、設案機能を 処理して引換をプリプレグシートを得た。これを実施例1に準じて設層し実施例1の場合 と同じサイズで成形した。

このものの ay は189 kg/mi 、 oたは1 4.1 kg/mp であつた。

#### 突旋例 5

水のかわりにメチルニルケトンに36%の エポマン付配を含む存在(硬化剤も含む、粘 及20でで35~A)を用いてジェット途を

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វាខា

次も付けた松は変យ例1と同様の業件で凝然 協議を処理して引揃えフリンレクシートを得 た。これを実施例1に単じて取居し、実施例 1の成形品と同じ寸法に成形した。このもの ののメは1945/m²、のまは7.6 kg/m²で あつた。

## 比較例 1

李越例1に用いた炭素観題を、水のジェット流を用いない以外は実施例1と同じ条件で処理し、待られた引摘をブリブレグシートを、35に実施例1に準じて福度し実施例1の成形品と同じ寸法に成形した。このものののメは195kg/mm®であつた。4. 四面の簡単を説明

第1 図はを発明の引物をブップレクの製造法の一乗越離機の工程説明図、第2 図は再圧流体を機構束に吹きつけるさいの製成の斜視図、第3 図~第5 図は各盤当て板の平面図、第6 図は円筒状の当て板を用いて総糖束にノメルから高圧流体を吹きつけている製費の正面図、第9 図

特別 昭52-151362 (6) は本発明の引御をプリプレグの概断面図及び第 8 図は従来品の引締とプリプレグの統断面図を 示す。

1、14、11:東

るゃくでおこフィリメント

5、34、54、56、54;当て板

4 1 、 6 2 、 6 5 1 押之ローラー

5 4、 6 0 : 穴

6、64:ノズル

7 こクリール

8:高圧ポンプ

9 : 受け亚

10:乾燥炉

11:会事的

12:0-9-

13: 加桑炉

1 4: 格取り器

等 所 出 版 人 工 想 技 宿 院 長 松 本 敬 信 ・ 日 本 カ ー ポ ン 株 式 会 社

Mr. Snider:

The data below belongs to the Fax sent on December 7, 2005. TOGAWA & LO.

(English Translation of Japanese Patent Application Laid-open No.52-151362)

A PRE-IMPREGNATION SHEET COMPRISING A PLURALITY OF MULTI-FILAMENT BUNDLES ALIGNED WITH EACH OTHER AND A METHOD OF PRODUCING THE SAME

# WHAT IS CLAIMED IS:

- 1. A pre-impregnation sheet comprising a plurality of multi-filament bundles aligned with each other wherein said bundles are uni-directionally disposed in parallel and one of some and most of monofilaments of said bundles respectively are intermingled with each other longitudinally along a moving course of said bundles and latitudinally with regard to said course and said monofilaments are impregnated with a resin.
- 2. A method of producing a pre-impregnation sheet comprising a plurality of multifilament bundles aligned with each other comprising the steps of uni-directionally disposing said plurality of multifilament bundles in parallel and blowing a high-pressurized fluid to a collection of said bundles in alignment and impregnating said collection with a resin one of when and after said fluid is blown over thereto.
- 3. A method of producing a pre-impregnation sheet comprising a plurality of multifilament bundles aligned with each other according to claim 2 wherein said fluid is one selected from water, mixture of water and air, an organic solvent and a synthetic resin.
- 4. A method of producing a pre-impregnation sheet comprising a plurality of multifilament bundles aligned with each other according to claim 2 or 3 wherein a pressure applied to said collection by said fluid ranges from 50 to 500 Kg/cm<sup>2</sup>.
- 5. A method of producing a pre-impregnation sheet comprising a plurality of multifilament bundles aligned with each other comprising the steps of uni-directionally disposing said bundles in parallel and blowing a high-pressurized fluid to a collection of said bundles from a nozzle reciprocally moving crosswise with regard to a moving course of said collection while continuously winding up said collection in alignment so

as to intermingle one of some and most of monofilaments of said bundles respectively with each other longitudinally along a moving course of said bundles and latitudinally with regard to said course and impregnating said collection with resin one of when and after said fluid is blown over thereto.

- 6. A method of producing a pre-impregnation sheet comprising a plurality of multifilament bundles aligned with each other according to claim 5 wherein said fluid is one selected from water, mixture of water and air, an organic solvent and a synthetic resin.
- 7. A method of producing a pre-impregnation sheet comprising a plurality of multifilament bundles aligned with each other according to claim 5 or 6 wherein a pressure applied to said collection by said fluid ranges from 50 to 500 Kg/cm<sup>2</sup>. (DETAILED DESCRIPTION OF THE INVENTION)

The invention relates to a pre-impregnation sheet comprising a plurality of multifilament bundles aligned with each other that is adopted for a forming material of a fibers reinforced plastic product.

The pre-impregnation sheet used for producing such plastic product is arranged such that non-woven fibers, yarn fibers, cloth fibers and chopped strand fibers, uni-directionally aligned fibers or such fibers as combining some of those fibers are impregnated with a thermoset resin, which pre-impregnation sheet as obtained has characteristics varied according to the type of fibers in use and is used in various fields according to such characteristics in need.

Among such sheets as mentioned above, that obtained by use of uni-directionally aligned fibers is easier to be formed into a thin sheet or tape shape so as to be optimum for the material for a tube-like body or a laminate plate and so forth so that it is adopted for such complex material of high strength as used for producing such sports or leisure goods as a golf shaft, a ski board and the assembly parts of automobiles and airplanes and the like.

Conventionally, such pre-impregnation sheet as mentioned

above is produced by impregnating uni-directionally aligned multifilament bundles with a resin and disposing in parallel a plurality of those bundles side by side so as to join the adjacent bundles with the impregnation resin so as to be formed into a sheet or tape shape.

The pre-impregnation sheet as conventionally obtained is vulnerable to mechanical stress and thermal stress because the adjacent bundles are bonded together with a non-cured resin so that the bonding strength between the adjacent bundles is susceptibly weakened subject to such stress. As a result of it, as for such conventional pre-impregnation sheet as mentioned above, a long-time storage and a temperature change during storage cause a gap between the adjacent bundles or an interlayer between them to be spaced apart. Further, during transportation and the production of a final product by use of such pre-impregnation sheet, the bonding strength between the adjacent bundles is weakened owing to mechanical stress and thermal stress so as to facilitate a gap or space to be generated between them with detriment to the quality of such sheet and a final product as well.

The widthwise and longitudinal strength of a fibers reinforced plastic product produced bv forming pre-impregnation sheet comprising a plurality uni-directionally aligned multifilament bundles and curing the impregnation resin depends on the strength of the cured resin itself and the bonding strength between the cured resin and the fibers. As for such conventional pre-impregnation sheet as mentioned above, the bonding strength between the cured resin and the fibers is relatively weak so that the widthwise and longitudinal strength of a fibers reinforced plastic product with such conventional pre-impregnation sheet in use is poor. Especially, the strength of a final product obtained by use of such pre-impregnation sheet as a gap being generated between the adjacent bundles is deteriorated and its finished appearance is poor, in addition to which there occur a lot of inconsistency in quality among final products.

The invention is to provide a pre-impregnation sheet comprising a plurality of fibers bundles aligned with each other and a method of producing the same in which the bonding strength between the adjacent bundles is not deteriorated owing to mechanical stress or thermal stress and a gap is hard to be generated between those bundles.

The invention is to provide a pre-impregnation sheet comprising a plurality of fibers bundles aligned with each other and a method of producing the same sheet wherein during handling and transportation, in process or during storage, its quality is not deteriorated.

The invention is further to provide a pre-impregnation sheet comprising a plurality of multifilament bundles aligned with each other and a method of producing the same wherein the widthwise and longitudinal strength of a fibers reinforced plastic product is enhanced and there is no inconsistency in quality among final products.

The pre-impregnation sheet comprising a plurality of fibers bundles aligned with each other according to the invention is characterized in uni-directionally and adjacently disposing a plurality of multifilament bundles and crosswise intermingling and commingling the monofilaments of those bundles with regard to the longitudinal and latitudinal direction of the fibers bundles and impregnating the bundles as intermingled and commingled with a resin.

The multi-filament bundle in use herein is such that a lot of filaments are converged into a bundle, a yarn or tow comprising a bundle of continuous filaments being preferred herein.

The following conventional fibers are adopted for producing a pre-impregnation sheet according to the invention.

- (1) Organic fibers: nylon (in a line of polyamide); rayon (in a line of cellulose); vinylon (in a line of polyvinylalcohol) and so forth
- (2) Organic heat-resistant fibers: aromatic polymer; polybenzoimidazole; polyfluorocarbon; polyamide; phenol;

polyphenyleneoxodiazole; bisbenzoimidazobenzophenanthroline; polythiadiazole; polyphenylenetriazole; polybithiazole; polyimide and so forth.

- (3) Inorganic fibers: glass fibers; boron nitride fibers; alumina; silicone nitride fibers; asbestos; zirconium; silicone carbide; carbonaceous, graphite, flame resistant carbon fibers and so forth.
- (4) Metallic fibers: tungsten alloy; beryllium; copper alloy; ferric and aluminium fibers and so forth.
- (5) Complex fibers: boron fibers cored with tungsten fibers; boron carbide cored with tungsten fibers; silicone carbide fibers cored with tungsten and boron fibers and so forth.
- (6) Combination comprising more than two fibers as selected from the above (1) to (5), preferably, combined fibers with flexibility and softness.

In order to intermingle the monofilaments of the adjacent bundles and within the same bundle with each other, any adjacent bundles are overlapped one over another to be closely attached together uniform in thickness so as to be formed into a sheet-like or tape shape with a certain width and a high-pressurized fluid is blown to the surface of the respective bundles in alignment with the tensile force of 0.02 to 0.65 g longitudinally applied to the respective bundles to prevent them from being slackened during operation.

The high-pressurized fluid in use includes water, mixture of water and air, an organic solvent such as methylalcohol, ethylalcohol, acetone, toluene, methyl ethyl ketone and so forth and a synthetic resin. In case of synthetic resin being adopted for the fluid, preferably, the same resin as the impregnation resin is used. Upon spraying such synthetic resin, it is preferred to lower the viscosity thereof by heating the same or adding an organic solvent having compatibility with the resin in use or diluents with the exclusion of the organic solvent such as vinyl chrolide resin plasticizer, a higher boiling point solvent, polypropyleneglycole, stylene monomer and polyethylene.

In the case of water, mixture of water and air being adopted for the fluid, it makes blowing operation cost-saving and the relevant facilities structurally simplified as well as does without fluidal adjustment and contamination of job environment while in the case of organic solvent or synthetic resin being adopted for such fluid, it makes drying operation subsequent to blowing operation simplified or does without the former operation so that a matrix resin impregnation operation is performed following the blowing operation. Especially, where the synthetic resin being sufficiently blown to the respective bundles, it does without dipping them into a synthetic resin solution anew and the matrix resin is impregnated with the respective bundles only by pressing those subjected to blowing operation with the rollers.

Herein, a high-pressurized fluid is blown to the respective bundles surface from a nozzle disposed above such surface with an interval therefrom and crosswise with regard to the alignment direction of the respective bundles.

The size of a nozzle aperture, the interval between the nozzle and the bundles surface and the number of nozzles depend on the diameter of the respective monofilaments as well as the thickness of the fibrous layer, but as for the size of the nozzle aperture, it shall be 1 mm or below, preferably, ranging from 0.05 mm to 0.5 mm. The size of the nozzle aperture becoming larger than the above maximum value, a lot of monofilaments are intermingled with each other in simultaneous transposition so as to cause the respective bundles to be put into disorder, which makes the thickness of the respective bundles non-uniform with detriment to the effect brought by aligning the respective bundles with each other.

The interval between the nozzle aperture and the respective bundles surface depends on the pressure by which the fluid is blown to them, the relative moving speed of the respective bundles to the nozzle aperture, the diameter of the respective monofilaments and the thickness of the respective bundles and so forth, which interval preferably ranges from 1

to 15 mm.

The pressure by which the fluid is blown to the respective bundles depends on the size of the nozzle aperture, the interval between the nozzle aperture and the respective bundles surface, the relative moving speed of the respective bundles to the nozzle aperture, the diameter of the respective monofilaments and the thickness of the respective bundles, which pressure preferably ranges from 50 to 400 kg/cm<sup>2</sup>. The pressure being less  $50 \text{kg/cm}^2$ , the transposition οf the respective monofilaments occurs scarcely so as to make the interengagement between the respective bundles insufficient while going beyond  $400 \, \mathrm{kg/cm^2}$ , a lot of fluffs occur along with the fibrous cut on the respective bundles.

Upon a high-pressurized fluid being blown over to the respective bundles surface, it may make them move in their alignment direction together with moving them crosswise with regard to their alignment direction with the nozzle fixed in a position while it may as well make the nozzle move with the respective bundles fixed in a position. The moving speed of either the nozzle or the respective bundles preferably ranges from 1 to 10 m/minute. Figure 2 shows a case where the respective bundles are under continuous treatment. As shown, they are endlessly wound up under a certain tension, whereupon the nozzle reciprocally moves crosswise with regard to the wind-up direction so as to discharge high-pressurized fluid towards the respective bundles surface.

The impregnation resin as adopted herein includes such thermoset plastic resins as phenol resin, non-saturated polyester resin, epoxy resin and such heat-resistant resins as polyimide resin, polybenzoimidazole resin, polyphenylen resin and friedel-crafts resin, which resins are heated or to which resins an organic solvent or diluent is added in order to lower the resinous viscosity.

Upon the high-pressurized fluid being blown over to the respective bundles surface, the provision of an abutment plate in the vicinity of the bottom side of the respective bundles

to which such fluid is blown over and in parallel with such surface enables the discharged fluid to be bounced back to be further put into contact with the respective bundles surface, which improves the efficiency of transposing the monofilaments of the respective bundles.

The abutment plate is smooth on the surface so as to throw back the discharged fluid and made from metallic, plastic, glass, wooden, hard rubber material and so forth, which plate is formed into a flat or cylindrical shape with no opening on the surface or may be provided with meshed opening or slit openings as shown in Figures 3 through 6.

The use of the abutment plate enables the respective bundles to be aligned with each other thereon and facilitates the holding means to hold the respective bundles with tension applied thereto to be disposed in a position so that the degree to which the respective monofilaments are intermingled with each other is adjustable in an arbitrary manner.

Then, the invention is explained with reference to the accompanying drawings on the basis of one embodiment to produce a pre-impregnation sheet comprising a plurality of multifilament bundles aligned with each other.

As shown in Figures 1 and 2, a group of respective multifilament bundles 1 aligned with each other is wound up by the wind-up drum 14 from the creel 7, which group is passed through the receptacle 9 with the respective bundles held by the tension control rollers 41, 42 and 43. During the respective bundles being in passage through the receptacle, high-pressurized fluid is blown over to the respective bundles surface through the nozzle 6 crosswise disposed with regard to the moving course of the bundles and with an interval from the respective bundles surface by driving the pump 8. The receptacle 9 is intended for receiving the fluid blown over to the respective bundles between the rollers 42 and 43 and is provided with an outlet which is not shown in the drawings to circulate the fluid back to the pump 8. Further, the receptacle 9 is provided with an abutment plate 3 disposed along the moving

course of the bundles, which plate is intended for throwing back the discharged fluid to the monofilaments of the respective bundles so as to enhance the transposition of the monofilaments or to make an efficient use of the fluid in use.

The abutment plate shall be arranged such that it throws back a high-pressurized fluid and is provided with physical strength enough to throw back the same. Figure 3 through 6 show such plate formed into a flat and a cylindrical shape. In the case of a number of openings being provided through a flat abutment plate, it facilitates such high-pressurized fluid to pass through the respective bundles so that the monofilaments of the respective bundles are transposed not only crosswise with regard to the moving course of the bundles, but also in the thickness direction of the bundles, which enhances them to be further intermingled with one another.

That is to say, Figure 3 shows a flat abutment plate 3a while Figure 4 showing a flat abutment plate 3b provided with slit openings 5b. Figure 5 shows a flat abutment plate 3c provided with meshed openings 5c. Figure 6 shows a side view of an apparatus wherein a high-pressurized fluid is blown over to the multifilament bundle 1d through the nozzle 6d with the cylindrical abutment plate 3d in use. The abutment plate provided with such openings is appropriate for the production of a pre-impregnation sheet larger in thickness.

Reference numeral 6 indicated in Figures 1 and 2 is a nozzle reciprocally moving crosswise with regard to the moving course of the respective bundles.

A multifilament bundles sheet produced by transposing the monofilaments of the respective bundles widthwise with regard to the alignment direction of the respective bundles and intermingling them with one another by the action of the high-pressurized fluid is moved to a drying chamber 10. Then, such sheet as dried is dipped into a resin impregnation tank 11 for bathing. Subsequently, such sheet as impregnated with a resin is treated with the roller 12 to make the impregnation operation complete and to adjust the amount by which such sheet

is impregnated with the resin. The sheet completed with the impregnation operation is further moved to a heating chamber 13 to volatilize the organic solvent component contained in the impregnation sheet and to enhance the polymerization and condensation of the impregnation resin so as to be wound up around a wind-up roller 14 as a pre-impregnation sheet comprising a plurality of multifilament bundles aligned and commingled with each other. The impregnation sheet to be heat-treated within the heating chamber is preferably sandwiched with releasing sheets.

As shown in Figure 7, the pre-impregnation sheet comprising a plurality of multifilament bundles aligned in parallel and commingled with each other is arranged such that the monofilaments existing between the respective bundles le and 1e and a part of or most of those monofilaments 2f within the same bundle are intermingled with each other so that the bonding strength between the respective monofilaments and the resin is not deteriorated by the action of mechanical stress and thermal stress differently from the prior sheet as shown in Figure 8, for which reason there occurs no gap between the respective bundles so as to prevent its quality from deterioration during handling and transportation, in process or during storage. The multifilament bundles sheet impregnated with a resin according to the invention being processed into a fibers reinforced plastic product, there scarcely occurs the deterioration of the fibrous strength in the longitudinal direction thereof. In comparison with the prior product, the fibrous strength both in the alignment direction and in the widthwise direction is intensified by 1.5 to 4 folds.

The preferred embodiment of the invention is described below on the basis of the following examples, to which examples the invention is not limited.

EXAMPLE 1

One hundred multifilament bundles respectively comprising 12,000 carbon monofilaments in the denier designation of 4800, the tensile strength and the elastic

modulus of which bundle are prescribed as 340 Kg/mm<sup>2</sup> and 20t/mm<sup>2</sup> respectively, are aligned with each other on a wooden flat plate with the tension of 0.10g applied to the respective bundles. Water jet stream subject to the following conditions is blown over to the respective bundles in alignment.

Water Jet Stream Conditions

Diameter of nozzle: 0.2 mm∮

Maximum pressure: 200 kg/cm<sup>2</sup> (40 spouts per minute)

Interval between the nozzle tip and the respective bundles

surface: 3 mm

Number of nozzle: one

Moving speed of the nozzle: 4.5 m/minute (moving crosswise with regard to the alignment direction with the jet air blown to the surface over 5 mm at a time to cover the whole width.)

Subsequent to the spraying operation of water jet stream, a part of carbon fibers as treated is sampled for checking the characteristics thereof, but there is no deterioration found in the tensile strength and the elastic modulus thereof in comparison with those checked prior to be subjected to the spraying operation.

There is no rupture strength in the widthwise direction between the bundles prior to the spraying operation, but posterior to such operation such strength works between them by the force of 200g/1 cm in width.

The pre-impregnation sheet as obtained above is dried for two hours under the temperature of 100 degrees Centigrade and dipped into an epoxy resin solution containing an organic solvent of methyl ethyl ketone, which sheet as impregnated with the resin is dried for 15 minutes under the temperature of 120 degrees Centigrade. The pre-impregnation sheets respectively having 0.1 mm in thickness are uni-directionally laminated one over another so as to be formed into a laminated complex sheet having the dimension of 150 mm in length and 80 mm in width and 3 mm in thickness. The tensile strength (oy) in the longitudinal direction of the complex sheet measures at 193 kg/mm² while that in the widthwise direction measures at 8.4 kg/mm². The ratio

by which the fibers are contained in the complex sheet amounts to 61 %.

## EXAMPLE 2

Under the same conditions as the example 1 excepting that the pressure of the water jet stream is set at  $400 \text{ kg/cm}^2$ , the respective carbon fibers bundles are treated so as to be formed into the respective pre-impregnation sheets, which sheets are laminated one over another so as to be processed into a laminated complex sheet having the same dimension as above. The tensile strength of the complex sheet in the longitudinal measures at  $189 \text{ kg/mm}^2$  while that in the widthwise direction measures at  $14.1 \text{ kg/mm}^2$ .

#### EXAMPLE 3

Under the same condition as the example 1 excepting that the jet stream comprises a solution containing epoxy resin by 35% and methyl ethyl ketone together with a curing agent, the viscosity of which solution measures at 25 cp at the temperature of 20 degrees Centigrade, the respective carbon fibers bundles are treated so as to be formed into the respective pre-impregnation sheets, which sheets are laminated one over another so as to be processed into a laminated complex sheet having the same dimension as that of the example 1. The tensile strength in the longitudinal direction thereof measures at 194 kg/mm² while that in the widthwise direction thereof measures at 7.6 kg/mm².

# COMPARISON 1

Under the same conditions as the above example 1 excepting that the water jet stream is not used, the respective carbon fibers bundles used in the above example 1 are treated so as to be formed into the respective pre-impregnation sheets, which sheets are laminated one over another so as to be processed into a laminated complex sheet having the same dimension as that of the example 1. The tensile strength in the longitudinal direction thereof measures at 195 kg/mm² while that in the widthwise direction thereof measures at 3.8 kg/mm².

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 shows one embodiment to carry out the method of producing a pre-impregnation sheet according to the invention; Figure 2 is a perspective view of an apparatus to blow high-pressurized fluid to the respective fibers bundles; Figures 3 through 5 show a plan view of an abutment plate in various shapes; Figure 6 shows a side view of an apparatus blowing a high-pressurized fluid over from a nozzle to the respective fibers bundles with a cylindrical abutment plate in use; Figure 7 shows the longitudinal plan view of a pre-impregnation sheet according to the invention while Figure 8 shows the corresponding view thereof according to the prior art.

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